The Combined Effects of Residual Stress and Warm Prestressing on Cleavage Fracture in Steels

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5 December 2012

Outline

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The Problem
The Chell Model
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Introducing Residual Stress
Using a Monte Carlo Simulation
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Introduction

Cleavage Fracture is one of the most severe and catastrophic types of failure found in ferritic Steel structures.

Warm Prestressing (WPS) is widely acknowledged as being able to enhance apparent material toughness especially in ferritic steels that exhibit lower shelf cleavage fracture.

Statistical analyses were carried out on experimental data provided by the Nuclear Research Institute (NRI) Řež, Czech Republic.

A Monte Carlo Simulation of a WPS model has been developed and applied to the NRI data and could be used to underpin the treatment of WPS in the R6 procedure.
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The Problem

The fracture mechanism of a ferritic steel is temperature dependent, **ductile** failure at high temperatures, and **brittle** fracture at low temperatures.

Neutron Embrittlement reduces the steel's Fracture Toughness, which effectively shifts the transition curve.

Significant scatter in Fracture Toughness affects the continuity between $K_{lc}$ and $K_f$. 
The Problem

- The fracture mechanism of a ferritic steel is temperature dependent, **ductile** failure at high temperatures, and **brittle** fracture at low temperatures.
- Neutron Embrittlement reduces the steel’s Fracture Toughness, which effectively shifts the transition curve.
- Significant scatter in Fracture Toughness affects the continuity between \( K_{lc} \) and \( K_f \).
What is Warm Prestress?

Warm Prestressing is widely acknowledged as being able to enhance a material’s toughness; increasing resistance to brittle fracture.

WPS effects are useful when considering accident scenarios, e.g. Loss-of-coolant-accidents (LOCA).
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Predicting WPS effect

- WPS - prior overload at a temperature higher than the transition and the subsequent operating temperature.
- Improvement in toughness caused majorly by:
  - Increasing in yield strength with decreasing temperature.
  - Formation of compressive residual stress field at crack tip.
- The Chell model relates the loading applied to a contour integral enclosing the associated plastic strain at the crack tip.
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Cool and Fracture (CF)

- CF loading regime used to determine original $K_{lc}$.
- Corresponds to Case 3 of Chell’s Model where the final loading step wipes out the effects of both Step 1 and 2.
- $S_2 < S_1 \leq S_3$
Load, Unload, Cool and Fracture (LUCF)

- LUCF loading regime involves unloading the preload prior to cooling.
- Corresponds to Case 1 of Chell’s Model where the plastic zone induced from preloading is the largest.
- \[ S_3 \leq S_2 < S_1 \]
Load, Cool and Fracture (LCF)

LCF loading regime involves the cooling process to occur immediately after preloading.

Corresponds to Case 2 of Chell’s Model where the final loading step wipes out the plastic zone induced by the unloading step.

\[ S_2 \leq S_3 \leq S_1 \]
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Generating ’Large Data’

Two factors highlight why comparisons cannot be made between individual specimens:

- Scatter found in the $K_{lc}$ data weakens assumption that specimens used for $K_{lc}$ and $K_{f}$ are the same, even though assuming same geometry and material properties.
- Lack of data implies that we don’t know the ’correct’ parameters associated with the distribution.

Parameters that best fit the data are determined and used in the Monte Carlo Simulation.
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Obtaining Parameters...

The statistical tool which provides the best fit to the scatter found in fracture toughness is a 3 - Parameter Weibull distribution.

\[ P_f = 1 - \exp \left( - \left( \frac{K - K_{\text{min}}}{K_0 - K_{\text{min}}} \right)^{m_K} \right) \]

Figure: 3 Parameter Weibull Fit
Obtaining Parameters...

- $m_K$ - Shape Parameter - dictates the shape of the distribution.
- $K_o$ - Scale Parameter - acts as a characteristic value of the distribution.
- $K_{min}$ - Threshold value - Corresponds to the value where the probability that a specimen will fracture is 0%.

*Shape* and *Threshold* can be fixed and the results are compared with that obtained from using the best fit parameters.
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Methodology

Experimental data was generated, at NRI for WWER 440 RPV steel, using single-edge-notched bend SE(B) specimens (pre-cracked charpy).

Data was partitioned into sub-groups in order to determine which parameter had the greatest effect on enhancing toughness.

- Fracture Temperature
- Warm Prestress Temperature
- Preload Level

Results are tabulated displaying the percentage certainty of WPS having a positive effect.
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Statistical Analysis of Experimental Results

**Figure: As-Received - LUCF - Comparing Preload Levels**

<table>
<thead>
<tr>
<th>Condition</th>
<th>Fracture Toughness (MPa m^0.5)</th>
</tr>
</thead>
<tbody>
<tr>
<td>CF N = 7</td>
<td>34.52 &lt; K \text{I} &lt; 45.87</td>
</tr>
<tr>
<td>LUCF N = 4 WPS (−80°C)</td>
<td>44.43 &lt; K \text{I} &lt; 93.12</td>
</tr>
</tbody>
</table>

**Figure: As-Received - LCF - Comparing Preload Levels**

<table>
<thead>
<tr>
<th>Condition</th>
<th>Fracture Toughness (MPa m^0.5)</th>
</tr>
</thead>
<tbody>
<tr>
<td>CF N = 7</td>
<td>30.9 &lt; K \text{I} &lt; 43.21</td>
</tr>
<tr>
<td>LCF N = 7 WPS (−80°C)</td>
<td>59.11 &lt; K \text{I} &lt; 76.04</td>
</tr>
<tr>
<td>LCF N = 8 WPS (−80°C)</td>
<td>59.11 &lt; K \text{I} &lt; 76.04</td>
</tr>
</tbody>
</table>
Outcomes

- The level of confidences obtained indicate clearly that Warm Prestress does indeed enhance the fracture toughness of this ferritic steel within statistical certainties.
- The confidence in demonstrating that there is a WPS effect was shown for $-180^\circ C$ - ranging from 91.6 - 99.6%.
- The Preload Level has a more significant effect than that of the WPS temperature.
- The Irradiated data exhibits the same pattern as the As-Received.
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- WPS model developed by Chell is used to predict the change in toughness after WPS and evaluate its accuracy.
- Monte-Carlo methods are used to predict the distribution in toughness following different warm prestressing cycles.
- 3 Parameter Weibull distributions were used to map not only the scatter observed in the $K_{lc}$ and $K_f$ data, but also the variation found in the preload level, $K_1$ data.
Chell Prediction using MCS Results

Figure: As-Received - CDF using best fit parameters with error bounds
Chell Prediction using MCS Results

**PDF at -140°C Fracture -- LUCF at 24°C**

- $K_c$ --- $m_K = 2.9735$, $K_o = 59.9061$, $K_{min} = 15.312$ --- Mean
- Experimental $K_f$ --- $m_K = 3.1754$, $K_o = 70.7157$, $K_{min} = 30.321$ --- Hazen
- Predicted $K_f$ --- $m_K = 3.2085$, $K_o = 72.1888$, $K_{min} = 26.63$ --- Hazen

**Figure:** As-Received - PDF comparing both types of parameters

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**MCS Results**

- Case 1
- Case 2
- Case 3

**Figure:** As-Received - display of the different cases occurring throughout the analysis
Outcomes

- The model predicts an increase in mean toughness increase to be within +/- 9% of the experimental value.
- The model provides a lower standard deviation compared with the experimental values.
- The best prediction was obtained from the group: Fracture Temp.\(\text{-}\)140\(^\circ\)C \emph{WPS24}\(^\circ\)C - higher degree of plasticity at 24\(^\circ\)C.
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Combining Residual Stress (RS) & Warm Prestress (WPS)

Different levels of unloading can be used to represent different levels of initial RS.

Obvious conclusion is that Tensile RS provides a benefit to WPS
Does the WPS relax the initial RS field?
Does the WPS relax the initial RS field?

Rate of RS relaxation depends on relative stiffness of cracked material to surrounding structure

At room temperature during preloading
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Monte Carlo Simulation of Structure

Figure: Statistical Variation of Toughness

Figure: Statistical Variation of RS
Monte Carlo Simulation of Structure

Stress intensity factor

Temperature

\( K_i \)

\( K_0 \)

\( K_1 \)

\( K_{10} \)

\( T_3 \)

\( T_1 = T_2 \)

\( K_f / K_{ic} \)

\( K_1 / K_{ic} \)
Monte Carlo Simulation of Combined RS & WPS

Figure: Without RS

Figure: With RS
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Conclusion

Test data from pre-cracked charpy specimens clearly demonstrated the effects of WPS.

A robust method for the statistical treatment of toughness data was established.

The Chell model provided a good level of accuracy when predicting the mean toughness increase, but did not provide the same accuracy for the spread of the distribution.

Predictions show that presence of high tensile residual stress provide an additional benefit from WPS to improvement in toughness.
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Looking Ahead...

- Experimental Programme - Further testing WPS effect with the presence of Residual Stress/Thermal stress.
- Attributing a level of significance to each parameter or physical effect, which acts to improve the toughness steel through WPS, would help to increase the accuracy of the model.
Thank you for listening...

ANY QUESTIONS?